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[54] Elastomeric silicone finishes and method of preparing same.

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⁽⁵⁾ An elestomeric silicone finish is prepared from a silicone system comprising a blend of silanois and crosslinable silicone intermediates. The blend is applied to the desired substrate and thereafter catalyzed and cured to obtain an elestomeric finish.

BACKGROUND OF THE INVENTION

1. Field of the Invention

This invention relates to a silicone system which provides an elastomeric silicone finish and methods of preparation thereof. The silicone system is prepared from a blend of silanols and crosslinkable silicone intermediates. This silicone system can be used in combination with other known finishing agents.

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2. Description of the Prior Art

Silicone products have been used extensively in the textile industry for more than twenty years as water repellents, antifoams,

- lubricants, softeners and the like. The most important silicone products have been dimethylpolysiloxane, used as a softener, and methylhydrogenpolysiloxane, used as the base for silicone water repellents.
- These silicone products, and others, have advantages over hydrocarbon compounds, paraffin waxes and fatty acid waxes, especially in regards to processing and the ultimate properties of the treated materials. Because of these advantages organosilicon polymers as textile chemicals were explored, resulting initially in U.S. Patent No. 2.891,920 which taught the manufacture of emulsion polymerized dimethyl polysiloxanes.

Some ten years later Weyenberg published a 30 written reference to organosilicon polymers in

t xtile chemicals. Journal of P lymer Science, Part C. No. 27 (1969). And more recently, the specific application of these silicone polymers as a textile finish has been made by Rooks in Textile Chemist and Colorist, Vol. 4. No. 1. Jan. 1972. The Rooks article specifically referred to the use of silanol endblocked dimethylpolysiloxane emulsion polymers with monomeric methyltrimethoxy silanes as the crosslinker and an organo tin catalyst. The Rook 10 article noted that the use of these ingredients in fortifying or improving the durable press performance of polyester/cellulosic blends was its most important application. However, this technology proved commercially unacceptable because 15 of its lack of consistency under mill conditions and the occurrence of silicone spots on the fabric.

Recently, an elastomeric silicone system
has been introduced as a textile finish. This
system is reported to impact improved resilience and
stretch, shape recovery and dimensional stability to
knitted and stretched woven fabrics. This silicone
system consists of three emulsion components, the
components are a high molecular weight silanol fluid
with a dimethylmethylhydrogen fluid correactant and
a zinc 2-ethylhexonate catalyst. The system is in
emulsion form, which limits the ability of
formulators to add value to the component materials
and is subject to critical operating conditions
which if not met could result in a dangerous

evolution of hydrogen.

Despite these recent advances there continues a need for a silicone system that provides

a better elastomeric finish that is easier to employ and which acts as a soften r by itself or can be used as a component in a durable resin bath. Additionally, the silicon system must be stable and impart formulation latitude so as to be acceptable across the spectrum of mill operations. Finally, it is important that the silicone system be easily catalyzed and preferably employ the same catalyst as found in a typical durable press resin bath.

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Summary of the Invention

A silicone system prepared from a blend of silanols and crosslinkable silicone intermediates. Said silicon system being capable to form a elastomeric film which functions as a softener, a water repellant and imparts resiliency and extensibility. Furthermore, the present silicone system can not only be used alone, but also finds great utility as a component in a durable press 20 resin bath. This silicone system is remarkably stable and provides a great amount of formulation latitude in textile finishes. Additionally, the elastomeric finish has been shown to provide a performance which can be varied by the degree of 25 functionality or molecular weight of the crosslinkable silicone intermediate. Catalysis for the present system is much less critical than previous systems in that any variety of acid catalyst can be employed in small amounts. Of 30 particular advantage is the fact that the present silicone system is catalyzed by any conventional durable press resin catalyst, thereby eliminating the need for a two-catalyst system.

Detailed Description of the Invention

In accordance with the present inventi n, there is provided a silicone system suitable to provide an elastomeric finish upon curing. The silicone system is prepared by reacting a silane and a silanol to obtain a crosslinkable silicone intermediate which is thereafter reacted with a second silanol to obtain a silicone composition which, when catalyzed, can be used as an elastomeric finish or coating for textiles, paper, cellulose materials, glass fibers and mineral substrates. The elastomeric finish or coating provides a film which is soft, resilient and durable. It is also believed that this film may impart lubricity and adhesive release properties.

The silanes which are suitable for use in preparing the crosslinkable silicone intermediate contain those generally represented by the formula:

wherein R is individually hydrogen. OR' or a substituted or unsubstituted hydrocarbon radical containing from 1 to 12 carbon atoms inclusive. preferably 1 to 3 carbon atoms and most preferably a methyl group, and X is R. OR' or

$$R_a$$

$$|$$

$$(C_nH_{2n})-Si-(OR')_{3-a}$$

30 and R' is individually a hydrocarbon radical containing from 1 to 6 carbon atoms, preferably from

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l to 3 carbon atoms. R' can be the same or different. The value of n is 1, 2, r 3 and preferably 2 and a is zero, 1 or 2. It is necessary that the silane contain at least 2 and preferably 3 alkoxy groups in order to provide a suitable crosslinkable silicone intermediate.

Illustrative of such silanes include, but are not necessarily limited to, methyltrimethoxysilane, silane, methyltriethoxysilane, ethyltriethoxysilane, methylpentamethoxyldisilylethane, tetraethoxysilane, cyclohexyltriethoxysilane, and methyltripropoxysilane tetraethoxysilane, cyclohexyltriethoxysilane, and methyltripropoxysilane, and methyltripropoxysilane.

Suitable silanols which can be used in the preparation of the crosslinkable silicone intermediate are these represented by the formula:

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wherein R'' is individually a hydrocarbon radical of from 1 to 12 carbon atoms inclusive and may be cyclic or noncyclic, saturated or unsaturated, branched or nonbranched, substituted or unsubstituted and wherein z has a value of from 10 to 500 and preferably having a value of 15 to 150. The commercially available silanols are predominately disilanols, but may certain small amounts of mono- and poly-silanols.

For the purposes of the present invention, it is preferred that the silanol be a dihydroxy endblocked dimethyl polysiloxane.

Th reacti n between th silane as represented by Formula I and the silanol as represented by Formula II takes place under conditions which are not strictly critical. Broadly, however, the reaction will occur within a temperature range of from to 70° to 120°C. Higher and lower temperatures may be employed but are not preferred. A nitrogen purge to remove any alcohol byproducts and unreacted silane ester is 10 recommended, although it is not criterial to the reaction. The reaction product is then heated at reduced pressure to remove all volatile products. Along these lines, time and temperature will affect the reaction rate but are also not strictly 15 critical. What is required in determining reaction conditions are those conditions necessary to obtain a condensed product. The molar ratio of silane to silanol should, at a minimum, be stoichemetrically equivalent, which requires that there be 2 moles of 20 silane per mole of silanol to get a double end-blocked crosslinkable silicone intermediate. No known adverse effect is believed to exist, however, when single end-blocked crosslinkable silicone intermediates are obtained.

It is very important that when the reaction is run only one of the alkoxy groups is removed. To accomplish this specific catalysts are highly recommended. Illustrative of such catalysts which can accomplish this feat are potassium carbonate sodium methoxide and potassium acetate preferably potassium carbonate.

The resultant crosslinkable silicone int rm diate is generally represent d by the formula:

$$R'O \xrightarrow{R} SiO \xrightarrow{R'} SiO \xrightarrow{R} Si \longrightarrow OR' (III)$$

wherein X, R, R' and R'' and z are all as previously defined.

The crosslinkable silicone intermediate represented by Formula III is subsequently mixed with a second silanol to obtain the blend which will subsequently be catalyzed and cured. Suitable silanols for this subsequent step are those of the general formula:

HO
$$\frac{1}{\sin y}$$
 H (IV)

wherein R''' individually has the same designation as that previously set forth for R'' and wherein y equals 185 to 3500 preferably 750 to 3500. It may be possible to employ silanols where y is greater than 3500, but such silanols are not preferred due to processing difficulties.

It should be pointed out that the silanol of Formula II and the silanol of Formula IV can be interchanged. Although this will increase the viscosity of the crosslinkable silicone intermediate, it is believed to be useful for the purposes of the present invention. If such

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int rchanges d ccur, it will be n c ssary when blending the cr sslinkabl silicone interm diate with th subs quently add d silanol t use a ratio f from 10 parts to 75 parts by weight of the crosslinkable silicone intermediate for every 90 to 25 parts by weight of the subsequently added silanol respectively.

In the event the interchange previously mentioned does not occur the weight ratio of crosslinkable silicone intermediate to subsequently added silanol should be from 10 to 50 parts by weight of the crosslinkable silicone intermediate to 90 to 50 parts by weight of the subsequently added silanol respectively.

The selection of a value for z and y in the silanols represented by Formulas II and IV respectively is made to meet the specific requirements in performance properties, such as flexability, resiliency and durability, of the ultimate elastomeric finish. The lower the value of z and/or y, the more brittle and less elastic the ultimate finish will be, conversely the higher the value of z and/or y, the more elastic the ultimate finish will be. In this manner formulators can with ease and convenience control the finish applied to the end products.

In the normal application of a finish, such as a textile finish, the crosslinkable silicone intermediate and the second silanol are preferably emulsified. This, however, is not a critical limitation insofar as nonemulsified blends of the crosslinkable silicone intermediate and silanol in

Curing is accomplished by any of a variety of methods commonly known to those skilled in the art. A curing method commonly mployed is a h ating oven whereby the finish is cured onto a d sired substrate.

In one embodiment of this invention, treatment of the textile material with the elastomeric finish of the present invention and treatment with a durable press resin (also known as "creaseproofing agent" or "textile resin") are carried out together, i.e. in the same bath. The durable press resins are known in the art and include aminoplast resins, epoxides, aldehydes, aldehyde derivatives, sulfones and sulfoxides. Aminoplasts are preferred durable press resins as they are relatively inexpensive. Suitable durable press agents are disclosed in "Crease-proofing Resins for Wash-and-Wear Finishing" by A. C. Nuessle, Textile Industries, Oct. 1959, pp. 1-12.

Typical aminoplast durable press resins include the urea-formaldehyde condensates. e.g. methylolated ureas and alkyl ureas; melamine-formaldehyde condensates. e.g. tri. tetra and penta methylol and methoxymethyl melamines.

25 etc.: alkylene ureas. e.g. dimethylol ethylene or propylene urea. dihydroxydimethylol ethylene urea and various alkoxymethyl derivatives thereof; carbamates. e.g. dimethylol alkyl and alkoxyalkyl carbamates. etc.: formaldehyde-acrolein condensation products: formaldehyde-acetone condensation products: alkylol amides. e.g. methylol formamide, methylol acetamide. etc.: alkylol acrylamides. e.g.

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the presence of a catalyst will work. When an mulsion syst m is employed the mulsifi r can be nonionic, cationic r anionic, preferably a nonionic emulsifi r is us d. Exemplary of nonionic emulsifiers include, but are not limited to, alkylphenol ethoxylates, primary and secondary alcohol ethoxylates, polyoxyethylene lauryl ethers. Exemplary of the anionic emulsifiers are alkyl benzene sulfonates, sodium lauryl sulfate. 10 Exemplary of the cationic emulsifier is trialkyl ammonium chloride.

The elastomeric finish is prepared by applying to the substrate, be it textile, paper, fiberglass or other, a blend or emulsion together with catalyst and, optionally, any other suitable finishing component and thereafter curing the coating onto such surface. Suitable catalysts which can be added to the blend of crosslinkable silicone intermediate and second silanol include those 20 commonly referred to as acid catalysts. Illustrative of such catalysts include, but are not necessarily limited to, the metal salts of strong acids, e.g. zinc nitrate, aluminum sulfate, zirconium acetate or zinc sulfate; metal halides, 25 e.g. zinc chloride, magnesium chloride, aluminum chloride; metal soaps, e.g. zinc-2-ethylhexoate, dibutyltindilaurate or dibutyltin diacetate; non-polymeric anhydrides, e.g. tetrapropenyl succinic anhydride; and butyl acid phosphate. 30 catalyst should preferably be added to the blend and/or emulsion and thus would not be present when the emulsion or blend is made to obtain optimum shelf life.

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N-methylol methacrylamide, N-methylol-N-methylacrylamide, N-methylol methylene-bis(acrylamides), methylen bis(N-methylol . acrylamide), etc.; diureas, e.g. trimethylol and tetram thylol acetylene diureas, etc.; triazones, e.g. dimethyl N-ethyltriazone, N.N'-ethylenebis(di-methylol triazone) and urons. e.g. dialkoxymethyl uron,

Typical epoxide durable press resins include the diglycidyl ethers of polyols such as 10 ethylene glycol diglycidyl ether and diepoxides such as vinyl cyclohexene dioxide. Typical aldehyde creaseproofing agents include formaldehyde, glyoxal and alpha-hydroxypivaldehyde. Typical aldehyde derivative creaseproofing agents include 15 2,4,6-trimethylol phenol, tetramethylol acetone, diethylene glycol acetal and pentaerytheritol bis acetal.

When the durable press resin and the elastomic finish of the present invention are 20 applied to the textile material from a single bath. a cure catalyst for the durable press resin is generally employed. The choice of catalyst is governed by the particular durable press resin. way of illustration, catalysts such as magnesium .25 chloride, zinc chloride, zinc nitrate, zirconium acetate, and amine hydrochlorides can be used with aminoplasts. Moreover, the catalyst suitable for curing the durable press resin will also cure the elastomeric finish. The cure of the durable press 30 resin is usually effected at an elevated temperature (e.g. from 150°C to 175°C) and the durable press

resin and the elastomeric finish of th present inventi n can thus convenintly b simultaneously cured.

The treatment of this invention can be employed in conjunction with any other treating steps and treating materials which are conventionally employed in the textile finishing art.

Whereas the exact scope of the instant invention is set forth in the appended claim, the following specific examples illustrate certain aspects of the present invention and, more particularly, point out methods of evaluating the same. However, the examples are set forth for illustration only and are not to be construed as limitations on the present invention except as set forth in the appended claims. All parts and percentages are by weight unless otherwise specified.

EXAMPLES

- Fabric Identification (Test Fabrics I) 20 Inc., Middlesex, NJ) 100% texturized polyester double A) knit jersey: style 720 25 100% bleached cotton single knit. B) sport shirt weight, style 459 50/50 = Polyester/cotton single C) 30 knit, tubular, style 7421 65/35 = Polyester/cotton woven D) fabric. Type 190, 3 oz./yd²
- 35 The procedural evaluations were run in accordance with the following AATCC and ASTM test methods.

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To a 1000 ml. 3 necked round bottomed flask equipped with a magnetic agitator, a thermometer fitted with a Therm-O-Watch regulator, an inlet tube for nitrogen and a distillation column packed (18) 457 mm 6.35 mm with (1/4") glass helices and fitted with a distillation head, receiver and vent to the hood via - 80°C cold traps, there was charged:

siloxane) having the following properties; wtt OH:

mPa·s

1.69, viscosity 54.1 (cs.) at 25°C; 81.6 g

MeSi(OMe)₃ at 99.7t purity; 4.4 g pulverized

K₂CO₃ anhydrous. The system was heated to 85°C

with agitation and (0.2 ft³)H₂/h. until 1 mole

ethanol per mole of MeSi(OMe)₃ charged was

removed. Treated 18 hours at 90°C with (0.5 ft³) 14.15 m³

N₂/h purge. The crude reaction product was then

vacuum stripped at 100°C/(0.2 mm) to remove all

volatiles. The compound was refined by pressure

filtration through a 1-2 μm pad.

The 'MD₂₇M' compound had the following properties:

Viscosity cs. @ 25°C 30.0 25

n_D 1.4013

25 Wt% methoxy:
found 5.3
calculated 5.8
Residual silanol <200 ppm

30 IR Spectroscopy: Spectrum consistent with anticipated structure showing disappearance of silanol absorption and appearance of SiOMe at 2840 cm⁻¹.

II) Test Procedures .

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- A) Evaluation f Wettability, AATCC M thod 79-1979
- B) Elmendorf Tear Resistance, ASTM Method D-1424-75
 - C) Conditioning Textiles for Testing, ASTM Method D-1776-79
 - D) Applicator: Werner Mathis Padder, Model VF-9779
- E) Wash Cycle
 Kenmore Machine Model 29601
 4# Load
 95 g A² TC² Detergent
 124/Cycle
 Medium water level
 Wash/rinse cycle = (120°F/105°F) 49/40°C
 - F) Dry Cycle

Kenmore Dryer, Model 7218601W 25 25 in @ "Normal" setting

The invention can be used for the preparation of a remarkably stable emulsion of two reactive intermediates which when catalyzed produced a crosslinked network which encapsulates or reacts with textile, cellulosic, glass fiber, mineral substrates. Crosslinking is achieved via water evaporation and a short elevated temperature catalytic cure.

Experimental

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Example I

Me Me We 1 40 (MeO)₂SiO-(Me₂SiO)₂₇ Si(OMe)₂ Preparation

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Gel Permeation Chromatogram: Molecular weight distribution in full agreement relative to starting silanol endblocked fluid.

5 Example II

Additional examples of polyalkoxy endblocked dimethyl silicones were prepared in a manner essentially identical to that described in Example I.

Table I summarizes all methoxyendblocked silicones prepared and their properties. Table II lists the reagents to prepare these compounds. The stoichiometries employed are calculated on the basis of 2 moles of polymethoxy silane per mole of silanol fluid. In the cases where MeSi(OMe)₃ was used, a 20-50% excess was employed to compensate for volatility losses.

TABLE I

Polymethoxy Endblocked Dimethyl Silicones and Their Properties

THE CO	טווטק			V T	de
79T (a)	Pino		25	Methoxy	Content
Code No. Formul	Formula	Visc. b	0	Found	Calculated
4	'MD27M'	30	1.4013	5.3	5.8
æ	"MD27M"	72	1.4071	9.2	10.1
ڻ	"MD112M"	195	1.4032	1.3	1.5
. Д	"MD112M"	380	1.4045	2.7	2.8
ធ	""MD112""	510	1.4046	• • •	i

Residual silanol content in all preparations = less than 200 ppm.

⁽a) CSI - crosslinkable silicone intermediate (b) in cps) at room temperature

TABLE II

Reagents Used to Prepare Polymethoxyendblocked Dimethyl Silicones

ပ်	Compound	יטטיא		S	Silanol Fluid	pid
	V24	233	Silane g Composition	6	Visc. (cps) mb. 4 wet OH	2.4 WEB
'MD27M' 4.4	4.4		81.6 Me~Si(OMe) ₃	503	54.1	1.69
"MD27M" 4.7	4.7		Me 127 (MeO) ₂ SiC ₂ H ₄ Si(OMe) ₃	503	54.1.	1.69
'MD ₁₁₂ M" 0.65	0.6	10	4.9 MeSi(OMe) ₃	103.8	144	0.75
"MD ₁₁₂ M" 1.1	1.1		ме 6.35 (MeO) ₂ S1C ₂ H ₄ S1(ОМе) ₃	103.8	144	0.75
""MD ₁₁₂ M"" 0.5	0.5		6.75 (MeO) $_3$ SiC $_2$ H $_4$ Si(OMe) $_3$	103.8	144	0.75

Formula Code:

$$D = Me_2 sio -$$

silane, was produced by the Pt catalyzed reaction of MeSiHCl₂ with ViSi(OMe)₃, esterified with methanol an refined via distillation. The compound

20 methanol an refined via distillation. The compound has the following properties:

Boiling Point

55°C(0.3 mm Hg) 0.4 mbar

1.4104

25 Isomer ratio (wt%):

Example III

Preliminary crosslinking studies were conducted by casting acid catalyzed dilute solutions and emulsions of the crosslinkable silicone

intermediates (CSI) with and without blends of silanol fluids having viscosities of 1,000-50,000 mm²/s (cs.) in laboratory test aluminum cups. In all cases acid catalysis was required for crosslinking to occur. Butyl phosphoric acid (BPA) is highly effective since it is compatible both in oil and water phases. The best elastomeric films were obtained when silanol fluids were admixed with the CSI in ratios of 25/75, 50/50 and 75/25. When the CSI fluid itself was tested a highly crosslinked.

friable silicone film was obtained that was deemed unsatisfactory as a textile elastomeric finish.

Concentrated nonionic emulsions of CSI and CSI/silanol fluid blends were prepared using the following materials/procedures.

There was mixed 35.0 g of CSI/silanol fluid slowly into a solution of 1.75 g of a nonionic surfactant composed of a blend of polyoxyethylene lauryl ethers and 1.75 g H₂O in a plastic beaker. After mixing well 61.35 g water were added until the emulsion was prepared. The emulsion was stabilized by adding 0.1 g. 37% formalin solution and 0.05 g NaHCO₃. The pH was adjusted to 5.5 with acetic acid. This 35% active emulsion was diluted with tap water to provide dilute test solutions.

The effect of temperature on crosslinking emulsions of 15-50% CSI/85-50% silanols respectively to provide elastomeric films gave the following

r sults when 2% BAP catalyst (based n silicon s lids) was emply d. Emulsions c mprised of 15/85 and 25/75 mixtur s of CSI Code A and 20,000(cstk) mm²/s silanol gav elastomeric films when contacted 2 days at 25°C, 5 h urs @50°C or 4 hrs @100°C. Films from 50/50 mixtures on standing 2 days at 25°C gave an elastomeric film. At 50°C the 50/50 mixture film was dry and after 4 hours at 100°C, we observed a friable dry film showing excessive crosslinking.

Similarly, a 15/85 blend of Polymethoxy/8,000(cs.) mm²/s silanol fluid respectively gave elastomeric films when treated at the 3 temperature/time conditions. The results clearly show how elastomeric films can be produced from broad mixture ranges of CSI with silanol fluids of 8,000 - 20,000(cstk.) mm²/s.

Film forming properties of the liquid CSI were demonstrated by preparing 20% solutions of CSA Code C and CSI Code E in tetrahydrofuran and catalyzing with 5% butyl acid phosphate based on silicone. On standing overnight, the solvent evaporated leaving a film via a crosslinking mechanism. Accelerated cure rates were demonstrated via 1/2 hr treatment at 80°C. Blends comprised of 25/75, 50/50, and 75/25 CSI with silanol fluids (1.000-8.000(cs)) similarly gave films on standing at ambient conditions. A BAP catalyzed silanol control remained fluid showing no propensity for film forming.

Example IV

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Elastomeric properties were imparted to a variety of fabrics by treatment in a model textile bath which consisted of:

- 2.85 g 35% silicone emulsion (as p r Example III)
- 0.10 g butyl acid phosphate (10% in wat r)

97.05 g distilled water

Applications conditions were adjusted to achieve 100% fabric wet pick up which upon drying gave 1.0 wt% silicone deposited on the fabric. The dry fabric was cured for 1.5 minutes at 171°C.

Silicone durability on the fabric was determined by washing five times in a 0.15 wtt 49° C detergent (AATCC #124) solution at (120°F) for 30 minutes then rinsing at 105°C. Prior to physical property measurements all fabrics were conditioned at 50% relative humidity and (70°F.) 21°C.

Bleached 100% cotton knit, sport shirt weight, style 459 when treated with CSI/silanol fluid mixture gave durable improvements in dimensional stability and tear strength relative to the untreated control. Table III clearly shows linear shrinkage or gain has been diminished by 50% and furthermore, tear strength has been increased 15-20% even after 5 launderings.

TABLE III

100% Cotton Knit treated with CSI/Silanol Fluid Blends

Silicone Bath	e Bath	Dimentional	ional	•			
Components	ents	after 5 launde	stability, & after 5 launderings	Inde	ear Stre	Tear Strength (Grams)	(MB)
CSI (Code)	Silanol Fluid (Viscosity) (a)	course	wale	Course	wale	Course	wale
ی	0000						
)	0000	+12.3	-11.2	2200	0006	0.00	
Ω	8,000	о +			0000	2100	3000
c	6	0	-11.8	2100	3000	2200	3000
י	20,000	+9.6	-10.4	2100	3006	6	
Q	20,000	0 0 1			0000	7200	3000
5	-	•	9.07	2100	3100	2100	3100
1	7,000	+10.1	-10.6	2200	3100		
!	•	+17 4	6			2400	2900
		•	77.0	2500	2600	2300	2500

(a) (cps) at room temperature

Example V

100% texturized polyester doubl knit jersey, style 720 (Test Fabrics, Inc., Middlesex NJ) was similarly treated with the same finishing bath compositions used in Example IV. Improvements (17-20%) in durable tear strength were measured after 5 launderings. Refer to data in Table IV. It is to be noted that 100% polyester is dimensionally stable.

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TABLE IV

100% Texturized Polyester Knit

Silicone Bath Components Tear Strength (grams).

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	CSI	Silanol Fluid,	Ini	tial	5 was	hes
	Code	Visc. (a)	Course	wale	course	wale
20	C	8,000	2200	3000	2100	3000
	D	8,000	2100	3000	2200	3000
25	С	20,000	2100	3000	2200	3000
23	D	20,000	2100	3100	2100	3100
	D ·	1,000	2200	3100	2200	2900
		disk the same	2500	2600	2300	2500

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mPa·s

(a) (cps)at room temperature

Example VI

This example illustrates the improved tear strength achieved by treating 50/50 polyester/cotton

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single knit, tubular, Styl 7421 with a 1% silicone actives from treating emulsi ns comprised of 25 mpa.s parts CSI C de B CSI/75 parts 8.000(cps)silan 1. For completeness of data, three catalysts were individually tested and comparative data are recorded in Table IV after fabric washing 3 times. The bath components are listed below.

	Components		<u>Parts</u>	by Weig	<u>ht</u> .
		1	<u>. 2</u>	3	4
10	35% Silicone Emulsion	2.9	2.9	2.9	2.9
	BAP (10% in Water)	-	0.2	-	_
	Zn(NO ₃) ₂ (25% in H ₂ O)	-	-	0.4	
	Zr(OAC) ₂ (25%in H ₂ O)	-	-	-	0.4
15	Water	97.1	96.9	96.7	96.7

Table V also shows Lewis acids are effective curing catalysts retaining 80-90% of the applied silicone relative to 60% retention for the noncatalyzed control. The silicone loss before and 20 after washing was determined via atomic absorption for silicon. Table V also shows significant improvements in durable tear strength with up to 30% increase in the fill and 90% increase in warp directions.

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TABLE V

		Silic ne Loss	Tear	Strend	th, gra	ms
	CATALYST	After 3 Washes	<u>Initi</u>		3 wa	sh s wale
5	Control X (Silicone, no catalyst)	38	2600	3000	2500	3100
	Butyl Acid Phosphate + silicone	19	2500	3100	2400	3100
10	Zn(NO ₃) ₂ + silicone	10	2600	3000	2600	3000
	Zr(OAC) ₂ + silicone	22 .	2500	2900	2600	3100
15	Control Y (No Silicone, no catalyst)		2300	2100	2000	1600

Conditions

- 1) Fabric: 50/50 = Polyester/cotton, single knit tubular
 - 2) Silicone Applied: 25/75 = CSI Code B polymethoxy fluid/L9000(8000), 35% Emulsion.

25 Example VII

This example illustrates the remarkable stability of CSI/silanol fluid emulsions on storage. Silicone mixtures comprised of 25 pts. CSI Code C/75 pts. 8000 cs. silanol fluid and 25 pts.

OSI Code D/75 pts. 8000 silanol fluid were emulsified to 35% silicone actives as described in Example III and buffered with NaHCO3. These systems were stored at room temperature and were periodically observed for appearance and gas

chromatographically analyz d for fr e methanol content. The analytical results are displayed below.

Emulsion Stability Studies

5	Days Storage	25/75 CSI Code C/ Silanol wt% Free MeOH	25/75 CSI Code D/ Silanol wt% Free MeOH
	1	0.005	0.026
10	14	0.005	0.046
	28	0.01	0.075
	84	0.005	0.065

At this point there was no change in the initial appearance of the emulsions and the tests were terminated. Additional methanol was generated by KOH treatment of the emulsions thus conclusively showing the surprising stability of methoxy 20 endblockers in properly buffered emulsions.

Example VIII

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As in Example IV this example illustrates durable dimensional stability and tear strength 25 improvements for other CSI/silanol fluid systems at 1% silicone solids on 100% cotton knits. Example IV data was based on CSI having chain lengths of 112 dimethyl siloxy units and cured with BAP catalyst. This example was Zn (NO3)2 catalyzed and 30 containing CSI having chain lengths comprised of only 27 dimethyl siloxy units (relative to 112 dimethyl siloxy units for Example IV). The data in Table VI clearly show that after 3 washes the dimensional stability has been improved 50% (course 35 and wale) and the wale tear strength has increased

15%. These enhancements have been achieved for silicone systems based on 1000-50,000 cs. silanol fluids when blended with 10-50 wt% CSI as per the model finishing bath formulation and cure conditions.

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TEAR STRENGTH GRAHS, 3 WASHES	Course Wale	2300 2600		2200 3100				2200 3000				2100 3100
WETTABLEITY, T. BECONDS	SHES	-			NM		300	300	300		16.3	300
TETAN	INITIAL	~		410	w en		300	300	300		163	300
OHAL TY, 1	Wale	-21.9		-11.2	-11.4		-12.2	-12.1	-12.0		-12.1	-11.8
DIMENSIONAL STABILITY, 4 3 WASHES	Course	+17.1		+0.9	+10.8		+10.1	+12.4	+11.4	nds	6.64	100+
	TREATMENTS (8)	As Rec'd Fabric	1) 15/85 - CBI Code A/Bilanol Fluid	(1000) cs (8000) cs	(20H) GB (20K)	II) 15/85 - CSI Code B/Bilanol Fluid		(8000) C#	-	III) CBI Code B/Bilanol (8000 cs) Blends	10/90	25/75 50/50

Notes: a) Finishing Bath Formulations In Silicone Solids (BOMT)

CGI/Gilanol (35%) Parts by Weight 7.9 Trillogic Cat. (25%) 0.4 Distilled Water 96.7

b) Fabric Wet Pick-Up: 120% c) Dry/Cure: 11/2 win [171°C

Experimental IX

This example is illustrative of the broad applicability of imparting durable dimensional stability and tear strength improvements for wide 5 ranging CSI/silanol emulsion systems applied and cured into 50/50 polyester/cotton knits. Here tested were the same silicone formulae employed in Example VIII using Zn (NO₃)₂ as the curing catalyst. Table VII shows the composition of the 10 specific treating systems, the weight fabric wet pick up to provide 1% silicone solids, and the cure conditions. Again the data in Table VII clearly show that after 3 washes the course and wale tear strength was improved 25-30% and there was 15-20% improvement in dimensional stability.

Similar improvements were achieved using 1% BAP catalyst.

50/50 Polye	50/50 Polyester Cotton Knit		
TREATWENTS (a)	DIMENSIONAL BTABILITY, 3 WASHES Wale	TEAN GRAMS, COULS	BTRENGTH J WASHES Wale
As Reig'd Fabric	-11.7	1700	2100
I) 15/85 - C8I Code A/8ilanol Pluid			
611anol Fluid Visc. (1000) cs (8000) cs	1 1 1 50 0 6 11 1	2300	2800 2900 3900
	-7.9	2200	3000
II) 15/85 = CBI Code B/L9000			
811anol Floid Viso. (1000) cs (2001) cs (2011) cs	6 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	2100	2900 2700 2900
` `	-9.5	2500	3000
10/90 15/85 25/75 50/50		2500 2400 2200	2800 2700 3100 2800
Notes: a) Finishing Bath Pormulations 18 Silicone Solida (SOMF)	(4	Experimental E	Esulators
	Parts by Weight	Parts	ts by Weight
Experimental Silidon Emulaion (35%) En(NO)2 Cat., (25%) Distilled Water	0.00 0.46	20 4	fler 5
<pre>d) Dry/Cure Cycle: 11/2 min # 1 d) Pabric Wet Pick-up: 1191</pre>	171°C	WallCO ₃	0.03

Example X

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This example is illustrative of 50/50 polyester cotton knit treated with a durable press resin bath to which CSI/silanol fluid emulsion compositions have been added. The results clearly show the entire bath treating system has improved physical properties as well as imparting a desirable soft hand relative to the fabric as received and containing resin alone. Thus both CSI containing on 10 average 27 dimethyl siloxy units and endblocked with dimethoxy or tetramethoxy clusters were blended with 1,000 to 50,000 cs. silanol fluids and after emulsification. directly added to the durable press bath, co-cured with the durable press resin system 15 without additional catalyst. In addition, these silicone emulsion compositions can contain 10 - 50 wt% CSI solids, the balance being comprised of silanol fluids.

The data in Table VIII shows durable 20 dimensional stability has been improved 50% in both wale and course directions and the tear strength improved 30-40% relative to the untreated fabric. Relative to the 50/50 knit treated with resin only. there are dramatic improvements in both softness and 25 physical properties which are required for the fabric to be commercially acceptable.

Ale GRAMS, 5.2 2000 6.8 2000 6.8 2000 6.9 2000 6.9 2000 6.9 2200 6.9		DINENSIONAL STABILITY,	ONAL.	akar	4.00
1 Fluids	TREATHENTS-	J WASH	63	GRAMS,	3 WASHES
1 Pluids		a l	MALL	Course	VB10
1 Fluids -5.2 2000 10.0 -4.8 2000 10.0 -4.8 2000 10.0 -4.8 2000 10.0 -4.7 2000 10.0 -4.9 2000 10.0 -5.2 2000 10.0 -5.2 2000 10.0 -5.2 2000 10.0 -5.2 2000 10.0 -5.2 2000 10.0 -5.2 2000 10.0 -5.2 2000 10.0 -5.0 2200 10.0 -5.0	AM Rec'd Fabric	-1.4	-10.3	1700	2100
1 Fluids -4.8 2000 +0.9 -4.8 2000 +0.6 -4.4 1800 +0.2 -4.7 2000 +0.5 -4.9 2000 0.0 -5.2 2000 +1.1 -5.2 2000 +1.1 -5.2 2000 +0.5 -4.9 2000 +0.5 -5.5 2000 +0.5 -5.5 2000 +0.5 -5.5 2000	Regin Only	+0.9		2000	900
1 Pluids					
1 Pluids	Silanoi Pluid ulan	•			
1 Fluids +0.9 -4.8 2000 +0.2 -4.7 2000 +0.2 -4.7 2000 +0.5 -4.9 2000 +0.5 -4.9 2000 +0.5 -4.9 2000 +0.5 -4.9 2000 +0.5 -4.9 2000 +0.5 -4.9 2000 +0.5 -4.9 2000 +0.5 -5.5 2000 +0.5 -5.5 2000 +0.2 -5.5 20	(1000) CE	6	•	0000	
1 Fluids +0.6 -4.4 1800 40.2 -4.7 2000 40.5 -4.9 2000 6.0 -5.2 2000 41.1 -5.2 2000 41.1 -5.2 2000 41.2 -5.0 2200 40.5 -4.9 2200 40.5 -4.9 2200 40.5 -4.9 2200 40.5 -4.9 2000 60.5 -4.9 2000 70.5 -4.0 2000 70.5 -		6.0+		2200	2000
Pluids +0.8 -5.0 2300 +0.5 -4.9 2000 0.0 -5.2 2000 0.0 -5.2 2000 +0.5 -4.9 2000 +0.5 -4.9 2200 +0.5 -4.9 2200 +0.5 -4.9 2200 +0.5 -5.5 2000 +0.5 -5.5 2000 +0.2 -5.5 2000 +		9.0+	7:	1000	2700
Fluids		***		2002	2800
Pa.s	II) 15/85 - CBI Code B/Bilanol Pluids	•			
Pa.s		. 0+	0.8	2300	
Cpm Blends +1.1 -5.2 2000 cpm Blends +0.6 -5.0 2200 +0.5 -4.9 2200 +0.5 -4.9 2200 +0.5 -5.5 2000 +0.2 -5.5 2000	_	+0.5	6.7-	2000	2200
Pars		٥.	72.5	2000	2400
cps Blends +0.6 -5.0 2200 +0.5 -4.9 2200 +0.5 -4.9 2200 +0.2 -4.9 2000 +0.2 -5.5		. 7 . 7	-5.2	2100	2800
10.6 -5.0 2200 +0.5 -4.9 2200 +0.5 -4.9 2100 +0.2 -5.5 2000 11ations Parts by Weight B) Dry/Cure 11/2 min (400) 14.0 C) Pabric We Pick-Ups 2.1 D) Silicons		•			
10.5 -4.9 2200 +0.5 -4.9 2100 +0.2 -5.5 2000 10.2 2000 10.2 2000 11/2 20	10/90	+0.6	-5.0	2200	2200
100 +0.5 -4.9 2100 +0.2 -5.5 2000 10.2 10.0 11.2 1	28/78	÷0+	6.7-	2200	2700
+0.2 -5.5 2000 liations	50/50	* O +	6.7	2100	2800
(400) 14.0 C) Parte by Weight B) Dry/Cure 11/2 min 11/2 min 14.0 C) Pabric We Pick-Up: 2.1 D) Silicone 10 solidary		+0.2	2.5	2000	2700
(400) 11/2 min 11/2 m	2	Parts	by Welght	ē	
(400) 14.0 C) Fabric We Pick-Up: 2.1 D) Silicone 10 action	Commenced Principle of the second Commenced			1	
Pick-Up: 2.1 D) Silicone 11 solida	İ		4.0	_	Wet L'
	Xn (NO3) 2 (251)		2.1	-	
			1		

Example XI

The properties of 65/35 polyester/cotton woven fabric. Type 190. (3 oz/yd) were improved by treatment with a durable press finishing bath containing CSI/silanol compounds as a elastomeric 5 softener component. Table IX lists the durable dimensional stability provided by the resin/silicon softener system relative to the as received fabric and the 100% improvements in durable tear strength relative to the durable press treated fabric alone. Illustrated in this example are the utility of 2,000 - 2,500 mol. weight dimethoxy and tetrmethoxy endblocked silicone fluids admixed with 1,000-50,.000 cs. silanol fluids which were added to 15 the treating bath as concentrated emulsions. The wt% polymethoxy endblocked silicone compounds co-cured with the durable press resin without the need for additional catalyst.

The tear strength of the silicone treated
fabric was doubled in both the fill and warp
directions. The hand was soft, smooth, and lively
relative to the durable press resin treatment
alone. These properties are required for fabric to
be of commercial utility.

TREATHERY STRENGTH	110018/88/81/ULEDOIS	A A CO DL KOE	D/PME88/511	anols
Fluids FILL WARP FILL -1.3 -3.0 -0.6 Fluids -0.5 -1.0 1400 Fluids -0.5 -1.0 1500 Fluids -0.5 -1.0 1500 Fluids -0.5 -1.0 1400 Fluids -0.5 -0.5 -0.5 Fluids -0.5 -0.5 -0.5 Fluids -0.5 -0.5 -0.5 Fluids -0.5 Fluids -0.5		DIMENSIONAL STABILITY,		STREMETS
1 Fluids -0.0 -0.8 700 -0.5 -1.0 1400 -0.5 -1.0 1500 -0.5 -1.0 1500 -0.5 -1.0 1500 -0.5 -1.0 1500 -0.5 -1.0 1400 -0.5 -1.0 1400 -0.5 -1.0 1400 -0.5 -1.0 1400 -0.5 -1.0 1400 -0.5 -1.0 1400 -0.5 -1.0 1400 -0.5 -1.0 1400 -0.5 -1.0 1400 -0.5 -1.0 1400 -0.5 -1.0 1400 -0.5 -1.0 1400 -0.5 -1.0 1400 -0.5 -1.0 1400 -0.5 -1.0 1500 -0.5 -1.0 140	TREATHENTS	£ .	-	3 WASHES
1 Fluids -0.0 -0.8 700 -0.5 -1.0 1400 -0.5 -1.0 1500 -0.5 -1.0 1500 -0.5 -1.0 1400 -0.5 -1.0 1	As Red'd Pabric		-	
1 Fluids -0.5 -1.0 1400 -0.5 -1.0 1500 -0.5 -1.0 1500 -0.5 -1.0 1500 -0.5 -1.0 1400 -0.5 -1.0 1	11100	•		•
Fluids				9
Pluids		•		
Pluids	Silanol Fluid Visc.	•		
Fluids	(1000)	10		
Fluids	_			1200
Fluids				1100
1400	15/85	;		7700
1400				
Apple Appl				1100
Cops Billicons Cops Cops Billicons Cops Cops Billicons Cops				1200
(qps Blends -0.5 -1.0 1400 -0.5 -1.0 1400 -0.5 -1.0 1400 -0.5 -1.0 1400 -0.5 -1.0 1400 -0.5 -1.0 1400 -0.5 -1.0 1400 -0.5 -1.0 1400 -0.5 -1.0 1400 -0.5 -1.0 1400 -0.5 -1.0 1400 -0.5 -1.0 1400 -0.5 -1.0 1400 -0.5 -1.0 1400 -0.5 -1.0 -0.5 -1.0 -0.5 -0.5 -0.5 -0.5 -0.5 -0.5 -0.5 -0	5			7200
-0.5 -1.0 1400 -0.5 -	CBI Code B/Silanol	•		7700
-0.5 -1.0 1400 -0.5 -				
1400	14/20			4000
1800	25/75			200
1400	50/50			1200
(401) Parts by Weight Pabric Wet (401) 14.0 14.0 15.0				1100
(354)	Pinishing Bath Formulations Durable Press Resin (408)	te by weight	1	
(354) 2.3 C) Dry/Cure Cyc (354) 2.3 D) 14 5414cone	## (BO-) - (-08-)			
(358) 2.3 b) 18 5111cone (804F)	TOTAL AND THE PRESENT OF THE PRESENT		Dry/Cure	izsi Yeles
(ANOS)	(351)		11/2 min 14 silico	~
	-	-	(BOMF)	

CLAIMS

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- 1. A process for imparting an lastomeric finish to a substrate which comprises:
- (a) applying to said substrate a silicone blend comprising:
 - (1) a crosslinkable silicone intermediate selected from the group of silicone compositions of the general formula:

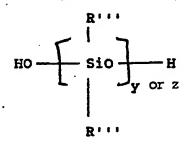
wherein R is individually hydrogen. OR' or a substituted or unsubstituted hydrocarbon radical containing from 1 to 12 carbon atoms;

R' is individually a hydrocarbon radical containing from 1 to 6 carbon atoms; and X is either R. OR' or

(C_nH_{2n}Si(R)_a(OR')_{3-a} wherein n is 1. 2 or 3 and a is 0, 1 or 2; z has a value from 10 to 500; and R'' is individually a hydrocarbon radical containing from 1 to 12 carbon atoms and may be cyclic or noncyclic, branched or nonbranched, substituted or unsubstituted, or saturated or unsaturated and

(2) a silanol selected from the group of silanols of the general formula:

D-13999



wherein R''' is individually a hydrocarbon radical containing from 1 to 12 carbon atoms and may be cyclic or noncyclic, branched or unbranched, substituted or unsubstituted or saturated or unsaturated and y has a value of from 185 to 3500; and

 $\hbox{(B)} \quad \hbox{$\tt $catalyzing and curing the} \\ \hbox{silicone blend onto the substrate} \; .$

- 2. The process of claim 1 wherein the substrate is selected from the group consisting of textiles, paper, cellulose materials, glass fibers and mineral fibers.
- 3. The Process of claim for 2 wherein the 20 silicone blend is applied to said substrate in an amount from 0.1 to 10 parts by weight per 100 parts by weight of untreated substrate.
- 4. The process of claim 1 wherein R is 25 hydrogen or methyl group.
 - 5. The process of claims 1 to 4 wherein R' is a hydrocarbon radical containing from 1 to 3 carbon atoms, preferably methyl.
 - 6. The process of claims 1 to 5 wherein R'' is methyl.

- 7. The process of claims 1 to 6 wherein X is R or OR' or $(C_2H_4)Si(OR')_3$ or $(C_2H_4)Si(R)(OR')_2$.
- 8. The process of claims 7 to 7 wherein z 5: has a value of from 15 to 150.
 - 9. The process of claims 1 to 8 wherein R''' is methyl.
- 10. The process of claims 1 to 9 wherein y is 750 to 3500.
 - 11. The process of claim 1 wherein the crosslinkable silicone composition is: